

DEPENDENCE OF THE SELECTOR DRUM ANGULAR VELOCITY AND LOAD ON THE TORQUE OF RESISTANCE FORCES FROM THE WINDING WIRE AND THE MOMENT OF INERTIA OF THE DRUM IN SECTION SELECTING

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Abstract

The analysis of the quality of winding on twisting machines has been carried out, the reasons for the formation and ways of eliminating winding defects and reducing the waste of raw materials during the processing of crepe yarns of natural silk have been established. Developed resource-saving technology for reducing silk thread winding defectiveness on twisting machines.

Keywords

winding, packing, silk, thread, density, twisting machine, winding defect, quality, waste raw materials, resource-saving technology.

INTRODUCTION

Improving the technological capabilities of warping machines installed at natural silk fabric production enterprises worldwide is considered a priority area of research for manufacturing knitted fabrics with high quality indicators and low raw material consumption. Extensive annual and long-term measures are being implemented to achieve these goals. In particular, the “Uzbekistan – 2030” Strategy outlines key objectives such as “efficient utilization of the local raw material base and development of industry based on advanced technologies” as well as “developing ‘driver’ sectors of industry and fully activating the industrial potential of regions.” In fulfilling these tasks, it is important, among other things, to improve the technology for developing resource-efficient silk crepe fabrics and to determine the rational parameters of the roving preparation drum in roving warping machines, thereby ensuring the competitiveness of export-oriented products manufactured by natural silk fabric enterprises.

This research work serves to a certain extent in implementing the tasks set forth in Decree No. PF-5989 of the President of the Republic of Uzbekistan dated

May 5, 2020, "On Urgent Measures to Support the Textile and Garment-Knitwear Industry"; Decree No. PF-60 dated January 28, 2022, "On the Development Strategy of the New Uzbekistan for 2022–2026"; Decree No. PF-71 dated May 1, 2024, "On Measures to Take the Development of the Textile and Garment-Knitwear Industry to a New Stage"; Decree No. PF-6 dated January 16, 2025, "On Additional Measures for Developing the Processing Chain in the Textile and Garment-Knitwear Industry"; as well as other regulatory and legal documents related to this field [2].

In the modern era of market relations, the most pressing development challenges for the silk industry are improving the quality of silk fabrics and enhancing their competitiveness in domestic and global markets by introducing innovative developments and technologies that ensure the production of high-quality products.

Silk is highly valued for its luster, durability, and excellent hygienic and performance properties. The use of natural silk threads in fabrics imparts softness and a unique, pleasant, delicate sheen, as well as excellent performance, hygienic, and consumer properties [3-4]. In the silk industry, the quality of products meeting international standards is largely determined by the quality of the silk threads, which in turn depends on the quality and properties of the cocoons.

The aim of this work is to develop an improved, resource-saving technology for reducing defects in the winding of silk threads on twisting machines.

METHODOLOGY

In textile processing technology, twisting plays a significant role in the efficiency of subsequent production processes.

The quality of yarn preparation for weaving is largely determined by the quality of the packages and the conditions under which the process itself is carried out, including the formation and preparation of the warp and weft yarns. The selection of these conditions and the optimization of the processes determine equipment productivity, the quality of products and semi-finished goods, waste yield, and the consumption of raw materials and materials.

Wang and Shi studied the problems of recycling silk textile waste [5]. Yan, Z., Yuyue, C.H., and Hong, L. investigated the production of silk thread consisting of two single yarns with different twist directions, which is treated with a calcium nitrate solution at 95°C to form a 3-D corrugated structure [6].

The structure and shape of the winding largely determine the strength of the package, the weight and length of the wound thread, the ability of the package itself to retain its shape and structure, as well as the conditions for winding the yarns in subsequent processing processes [7].

type of assortment. In the new technology, since the number of single threads selected at the same time is increased by 4 times (4 layers), the productivity also increases by 4 times, and the number of wicks is 4 times less.

By wicks and when grouping them, the change in mass is taken into account when calculating the value of the moment of inertia of the drum.

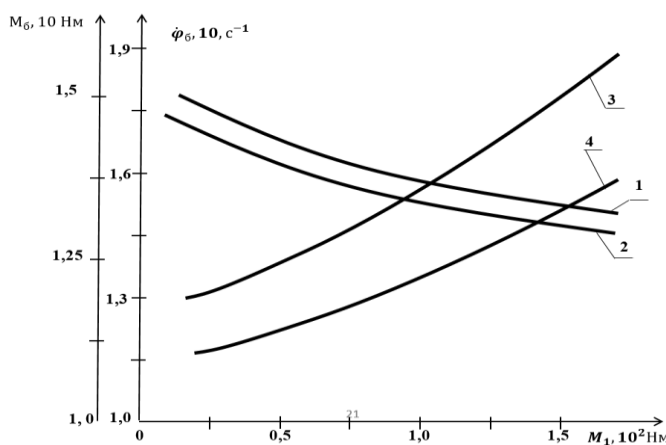
In this case, the drum, the motor rotor and other rotating masses are taken into account on the drum shaft and rotor.

It should be noted that with an increase in the coefficient of friction of the belt transmission transmitting movement to the wicking drum, the values of the coefficient of unevenness of its angular velocity decrease (Fig. 2). Here:

$$\delta_{\phi} = \frac{\dot{\phi}_{\phi \max} - \dot{\phi}_{\phi \min}}{\dot{\phi}_{\phi \text{пр}}} = \frac{2(\dot{\phi}_{\phi \max} - \dot{\phi}_{\phi \min})}{\dot{\phi}_{\phi \max} + \dot{\phi}_{\phi \min}} \quad (1)$$

where $\dot{\phi}_{\phi \max}$, $\dot{\phi}_{\phi \min}$ - maximum and minimum values of the angular velocity of the pick drum.

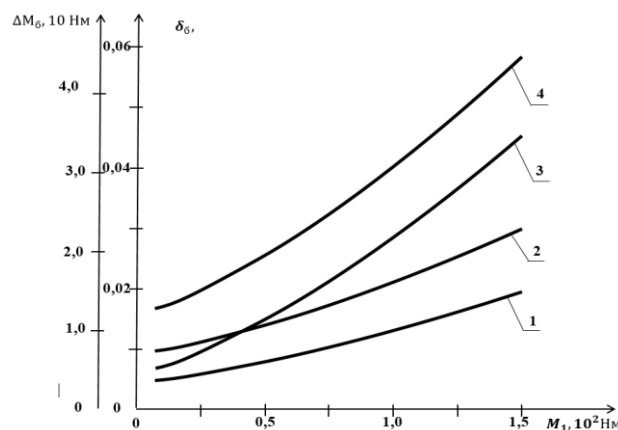
As a result of the obtained law of motion and processing of loads, the dependence graphs of the parameters were constructed. In particular, Figure 5 shows the dependence graphs of the angular velocity of the selector drum and the load on the moment of resistance forces coming from the winding yarn and the moment of inertia of the drum. According to the analysis of the graphs, when the technological resistance M_1 values are increased from $0.25 \cdot 10^2 \text{Nm}$ to $1.5 \cdot 10^2 \text{Nm}$ and $I_b = 2.5 \text{kgm}^2$, the angular velocity of the drum decreases in a linear fashion from 18.2s^{-1} to 14.9s^{-1} , while the values of the turning torque decrease in a linear fashion from $1.12 \cdot 10^2 \text{Nm}$ to $1.358 \cdot 10^2 \text{Nm}$. That is, as the resistance increases, the turning torque increases correspondingly, but the angular velocity decreases. Accordingly, as $I_b = 3.5 \text{kgm}^2$ increases, the values of $\dot{\phi}_{\phi}(b)$ decrease from 17.21s^{-1} to 13.92s^{-1} in the nonlinear coupling, and the values of M_b increase from $1.17 \cdot 10^2 \text{Nm}$ to $1.56 \cdot 10^2 \text{Nm}$.



$$1,2-\dot{\phi}_{\phi} = f(M_1); 3,4-M_b = f(M_1); 1,4-I_b = 2,5 \text{kgm}^2; 2,3-I_b = 2,5 \text{kgm}^2;$$

Figure 2. Graphs of the dependence of the angular speed and loading of the pick drum on the torque of the resistance forces coming from the winding thread and the moment of inertia of the drum

Accordingly, Figure 3 shows the dependence of the angular velocity of the selection drum on the unevenness coefficient and the torque of the screwdriver on the moment of resistance from the winding thread. The analysis shows that when the M_1 values increase to $1.5 \cdot 10^2 \text{Nm}$ and $C_t = 450 \text{ Nm / rad}$, the angular velocity of the selection drum increases from 0.0045 to 0.021 in a linear manner, while the torque of the screwdriver increases from 5.1 Nm to 31.3 Nm. Accordingly, when the unevenness coefficient is 250 Nm / rad , the values of δ_b increase from 0.009 to 0.032. In this case, the values of ΔM_b reach 44.3 Nm. Therefore, it is recommended not to exceed the technological resistance values $(1.0 - 1.2)10^2 \text{Nm}$ in order to reduce the fluctuation of the angular speed of the drum and to ensure that the torque does not exceed.

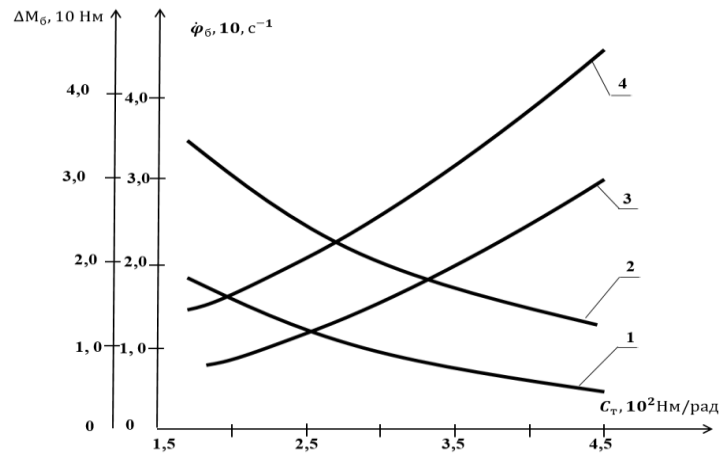


1,2- $\delta_b = f(M_1)$; 3,4- $\Delta M_b = f(M_1)$; 1,4- $C_t=450 \text{ Nm/rad}$; 2,3- $C_t=250 \text{ Nm/rad}$;

Figure 3. Graphs of the dependence of the angular velocity of the pick drum, the unevenness coefficient and the torsional torque vibration range on the torque of the resistance forces coming from the winding thread

Also shown in Figure 4 are graphs of the dependence of the angular velocity of the selection drum and the vibration range of the torque of the drill on the change in the belt transmission stiffness coefficient. According to the analysis, when the stiffness coefficient C of the belt mechanism transmitting motion to the selection drum increases from $0.8 \cdot 10^2 \text{Nm/rad}$ to $4.5 \cdot 10^2 \text{Nm/rad}$ and when $M_1=150 \text{ Nm}$, the angular velocity vibration range decreases from 1.8 s^{-1} to 0.38 s^{-1} , the ΔM_b values increase in a linear fashion to 44.6 Nm. Accordingly, when $M_1=120 \text{ Nm}$, the $\Delta \varphi_b$ values decrease from 3.32 s^{-1} to 1.22 s^{-1} , and the ΔM_b values increase to 28 Nm.

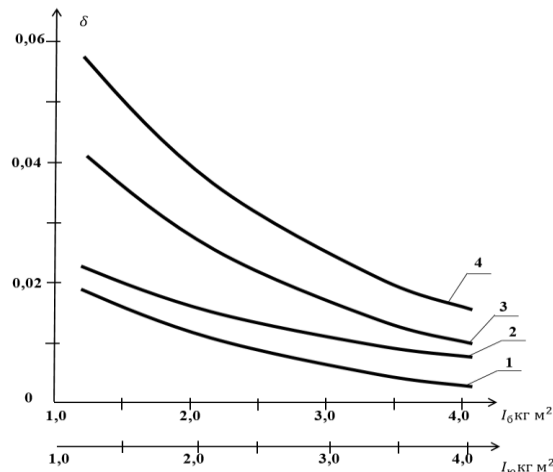
Therefore, to ensure smooth rotation of the body drum, the values of the belt drive friction coefficient are recommended to be in the range of $C_t=(400-420) \text{ Nm/rad}$.



$$1,2-\dot{\varphi}_6 = f(C_T); 3,4-\Delta M_b = f(C_T); 1,4-M_1 = 150 \text{ Nm}; 2,3-M_1 = 150 \text{ Nm};$$

Figure 4. Graphs of the dependence of the angular speed of the selector drum and the vibration ranges of the screwdriver torque on the change of the coefficient of uniformity of the belt transmission

It should be noted that the heavier the selection drum, the higher the moment of inertia, the smoother it rotates. Figure 5 shows graphs of the angular velocities of the selection drum and the drive (motor) rotor shafts against the corresponding moments of inertia.



$$1,2-\delta_{Yu} = f(I_{y0}); 3,4-\delta_b = f(I_b); 1,3-C_T=450 \text{ Nm/rad}; 2,4-C_T=250 \text{ Nm/rad};$$

Figure 5. Graphs of the dependence of the coefficients of unevenness of the angular velocities on the shafts of the selector drum and the rotor of the driver (engine) on the corresponding moments of inertia

According to the analysis of the constructed graphs (Fig. 5), when the moment of inertia of the masses applied to the driving rotor increases from 0.55 kgm² to 0.8

kgm², the values of δ_p decrease from 0.02 to 0.0034, and the values of δ_b decrease from 0.039 to 0.011 when the rotor angular velocity unevenness coefficient $C1=450$ Nm/rad. Accordingly, when the belt roughness coefficient is taken as 250 Nm/rad, the values of δ_p decrease from 0.024 to 0.01, and the values of the drum angular velocity unevenness coefficient δ_b decrease from 0.051 to 0.022 in a nonlinear relationship. Therefore, in order to reduce the values of $\delta_{\rho\alpha}$ and δ_{β} , and to ensure uniform rotation of the selection drum and the motor rotor, the recommended values of the moments of inertia are $I_p = (0.5-0.6)$ kgm²; $I_b = (3.0-3.5)$ kgm².

CONCLUSION

Thus, based on the results of the work, the following conclusions can be drawn. The effect of technological resistance on the dynamic parameters of the selection drum in the pre-selection was studied. As a result of the dynamic analysis of the drum of the pre-selection machine, it was theoretically determined that with an increase in the resistance from the winding yarn, the vibration amplitude also increases, and it was proved that the vibration frequency corresponds to the vibration frequency of the moment of resistance forces. It was found that when the technological resistance values in the pre-selection machine are increased, the angular velocity of the selection drum decreases in a linear manner, while the values of the turning torque decrease in a linear manner.

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